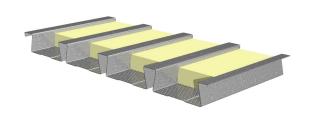
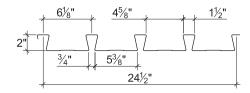
2.0DA ACOUSTICAL DOVETAIL ROOF DECK

- Enhanced 2-Coat Polyester Paint
- White Factory Primer Paint
- Galvanized Finish
- FM Listed



Nominal Dimensions





Section Properties

	Deck Weight	Base Metal Thickness	Yield Strength	Effective Moment of Inertia at Service Load I _d = (2I _e +I _g)/3		Effective Section Modulus at F _v = 40 ksi		Allowable Moment		Vertical Web Shear	
Deck Gage	w _{dd} (psf)	t (in.)	F _y (ksi)	l _d + (in⁴/ft)	l _d - (in⁴/ft)	S _e +	S _e - (in³/ft)	$M_n + /\Omega$ (lb-ft/ft)	M_n -/ Ω (lb-ft/ft)	V _n /Ω (lb/ft)	
22	2.0	0.0295	40	0.340	0.310	0.261	0.258	521	515	2896	
20	2.4	0.0358	40	0.415	0.385	0.330	0.317	659	633	3498	
18	3.2	0.0474	40	0.551	0.528	0.445	0.427	888	852	4584	
16	4.0	0.0598	40	0.697	0.684	0.564	0.546	1126	1090	5723	

Allowable Reactions at Supports Based on Web Crippling, R_n/Ω (lb/ft)

Bearing Length of Webs One-Flange Loading Two-Flange Loading End Bearing Interior Bearing End Bearing Interior Bearing Deck 2" 3" 4" 3" 5" 2" 3" 4" 3" 5" Gage 11/2" 11/2" 702 22 653 717 826 917 1281 1516 757 925 1877 848 1567 1823 20 931 1020 1170 1296 2146 1058 1136 1266 1376 2258 2690 18 1556 1697 1933 2132 3036 3544 1893 2023 2239 2422 3813 4507 16 2378 2582 2926 3215 4629 5360 3043 3237 3563 3837 5866 6880

Standard Features

- ASTM A653 SS GR 40 Min. with G90
- Standard lengths 6'-0" to 42'-0"
- Tables conform to ANSI/SDI RD-2017
- IAPMO UES ER-423 and FM Listed

Optional Features

- Inquire regarding cost and lead times for:
 - -19 gage
 - -Short cuts < 6'-0"
 - -Alternative metallic and painted finishes



2.0DA ACOUSTICAL DOVETAIL ROOF DECKGRADE 40 STEEL

Inward Uniform Allowable Loads, ASD (psf)

Spans Spans Criteria 4'-0" 5'-0" 6'-0" 7'-0" 8'-0" 9'-0" 10'-0" 11'-0" 12'-0" 13'-0" 14'-0" 12'-0" 13'-0" 14'-0" 13'-0" 13'-0" 14'-0" 13'-0"	Deck		Span (ft-in.)											
		Spans	Criteria	4'-0"	5'-0"	6'-0"	7'-0"	8'-0"	9'-0"	10'-0"	11'-0"	12'-0"	13'-0"	14'-0"
Double V _n / Ω 251 162 113 83 64 51 41 34 29 24 24 24 24 24 24 2	22	Single	W_n / Ω	260	167	116	85	65	51	42	34	29	25	21
			L/240			103	65	44	31	22	17	13	10	8
		Double	W_n / Ω	251	162	113	83	64	51	41	34	29	24	21
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			L/240									28	22	18
		Triple	W_n / Ω	311	201	141	104	80	63	51	42	36	30	26
20 $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		iripie	L/240					75	53	38	29	22	17	14
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	20	Single	W_n / Ω	329	211	146	108	82	65	53	44	37	31	27
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			L/240			126	79	53	37	27	20	16	12	10
Triple V_n / Ω 382 247 173 128 98 78 63 52 44 37 37 382 V_n / Ω 444 284 197 145 111 88 71 59 49 42 38 V_n / Ω 415 268 187 138 106 84 68 56 47 40 38 V_n / Ω 513 333 233 172 132 104 85 70 59 50 49 V_n / Ω 513 333 233 172 132 104 85 70 59 50 49 38 30 28 V_n / Ω 563 360 250 184 141 111 90 74 63 53 49 V_n / Ω 530 343 239 176 135 107 87 72 60 51 49 38 30 108 V_n / Ω 530 343 239 176 135 107 87 72 60 51 49 38 30 30 30 30 30 30 30 30 30 30 30 30 30		Double	W_n / Ω	309	199	139	102	79	62	50	42	35	30	26
Triple $\frac{1}{1240}$ 93 65 48 36 28 22 11 $\frac{1}{1240}$ 167 105 71 50 36 27 21 16 16 $\frac{1}{1240}$ 167 105 71 50 36 27 21 16 16 $\frac{1}{1240}$ 167 105 71 50 36 27 21 16 16 $\frac{1}{1240}$ 38 3 $\frac{1}{1240}$ 38 $\frac{1}{1240}$ 38 $\frac{1}{1240}$ 128 90 65 49 38 30 24 $\frac{1}{1240}$ 128 90 65 49 38 30 24 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 11 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 11 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 11 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 11 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 133 89 63 46 34 26 21 17 $\frac{1}{1240}$ 212 21 33 89 63 46 34 26 21 34 $\frac{1}{1240}$ 212 21 33 89 63 46 34 26 21 34 $\frac{1}{1240}$			L/240										28	22
		Triple	W_n / Ω	382	247	173	128	98	78	63	52	44	37	32
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			L/240					93	65	48	36	28	22	17
	18	Single	W_n / Ω	444	284	197	145	111	88	71	59	49	42	36
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			L/240			167	105	71	50	36	27	21	16	13
Triple $\frac{\text{L}/240}{\text{L}/240}$ $\frac{\text{L}}{240}$ \text		Double	W_n / Ω	415	268	187	138	106	84	68	56	47	40	35
Triple $\frac{1}{1240}$ 128 90 65 49 38 30 2 Single $\frac{W_n/\Omega}{L/240}$ 563 360 250 184 141 111 90 74 63 53 4 $\frac{L/240}{L/240}$ 212 133 89 63 46 34 26 21 1 $\frac{W_n/\Omega}{L/240}$ 530 343 239 176 135 107 87 72 60 51 4 $\frac{L/240}{L/240}$ 49 3 $\frac{W_n/\Omega}{L/240}$ 655 425 297 220 169 133 108 90 75 64 55			L/240										38	30
		Triple	W_n / Ω	513	333	233	172	132	104	85	70	59	50	43
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			L/240					128	90	65	49	38	30	24
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	16	Single	W_n / Ω	563	360	250	184	141	111	90	74	63	53	46
Triple $\frac{16}{L/240}$ $\frac{1}{240}$ $\frac{1}{$			L/240			212	133	89	63	46	34	26	21	17
Triple W_{n}/Ω 655 425 297 220 169 133 108 90 75 64 5		Double	W_n / Ω	530	343	239	176	135	107	87	72	60	51	44
Triple "			L/240										49	39
L/240 165 116 85 64 49 39 3		Triple	W_n / Ω	655	425	297	220	169	133	108	90	75	64	55
			L/240					165	116	85	64	49	39	31

Notes:

- 1. Table does not account for web crippling. Required bearing should be determined based on specific span conditions.
- 2. The symbol "---" indicates that the uniform allowable load based on deflection exceeds the allowable load based on stress.

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